

Thermal Recovery of Bitumen



LARICINA
E N E R G Y L T D.

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Thermal Recovery of Bitumen

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- 1. SAGD as a mechanism (instead of a process)**
- 2. How a Steam/Oil Ratio is Determined**
- 3. Optimizing Thermal Bitumen Recovery**

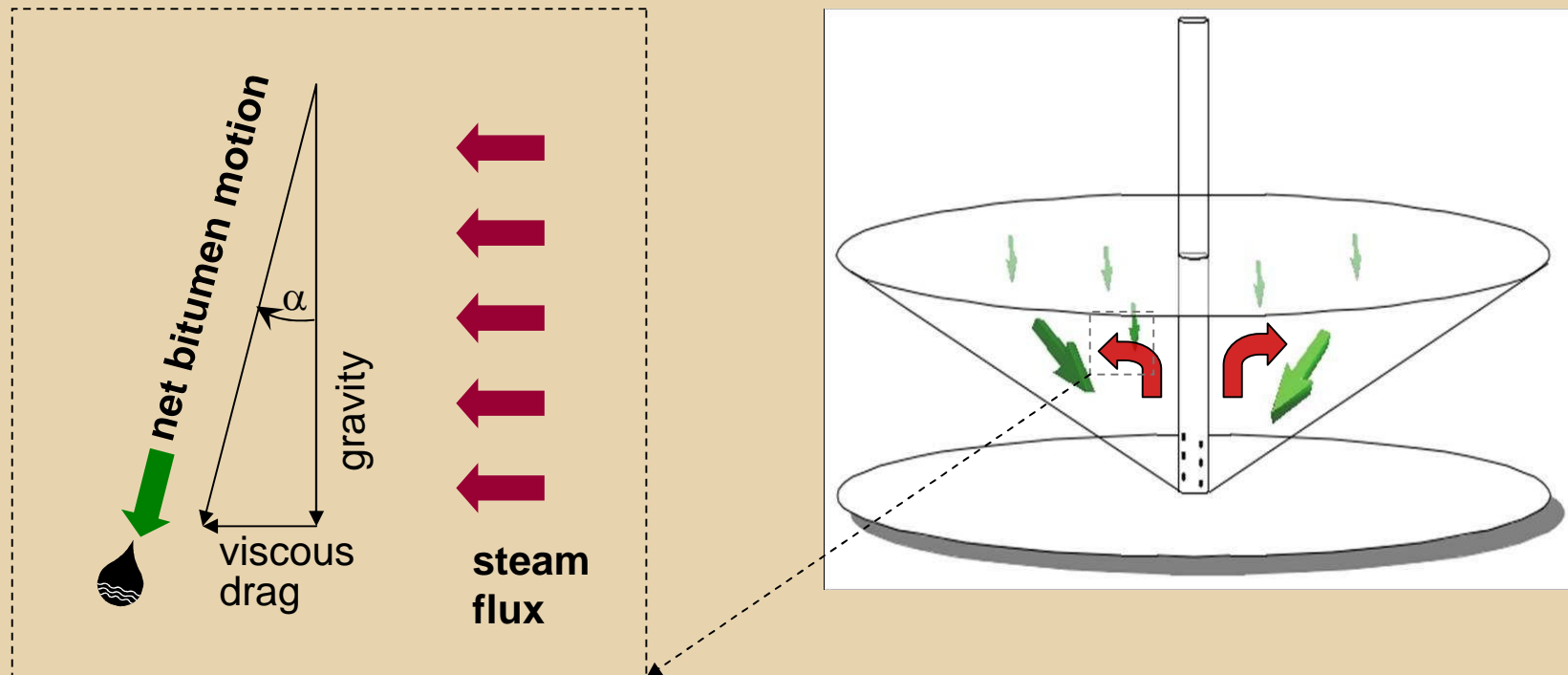
SAGD as a Mechanism

- By default, bitumen recoveries > 5-10% must be due to gravity:
 - *water is 100x more mobile @ 200C*
 - *oil:gas is gravity dominant, i.e. one or both phases will be moving vertically*
- physical understanding allows tailored application to reservoir circumstances

Gravity Drainage Requirements	
<i>requirement</i>	<i>methods</i>
oil mobility:	<ul style="list-style-type: none">•heat•solvent
permeability:	<ul style="list-style-type: none">•rock quality•dilation?
gas phase voidage:	<ul style="list-style-type: none">•steam•solvent•methane, etc.

Gravity Dominant Conditions

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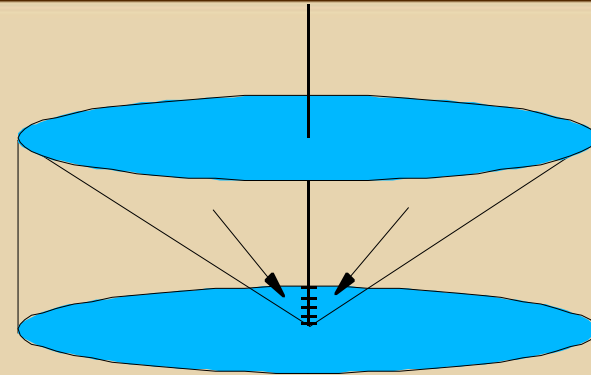


- the gravity vector (velocity of fall) is proportional to permeability
- the drag due to steam injection is inversely proportional to permeability
- above about 1 Darcy, gravity tends to dominate, & bitumen falls close to vertical

Gravity Depletion Geometries

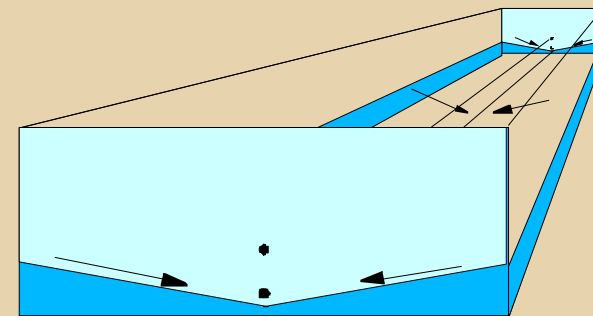
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- vertical wells tend to drain inverted cones
- horizontal wells drain trough-like shapes
- at the economic limit, horizontals recover ~2.5x more oil from same heated area



Vertical CSS (i.e. radial, cyclic SAGD):

- 1/3 sweep @ 10 years (typ.)
- $1/3 * (.85-.15) = 23\%$ recovery

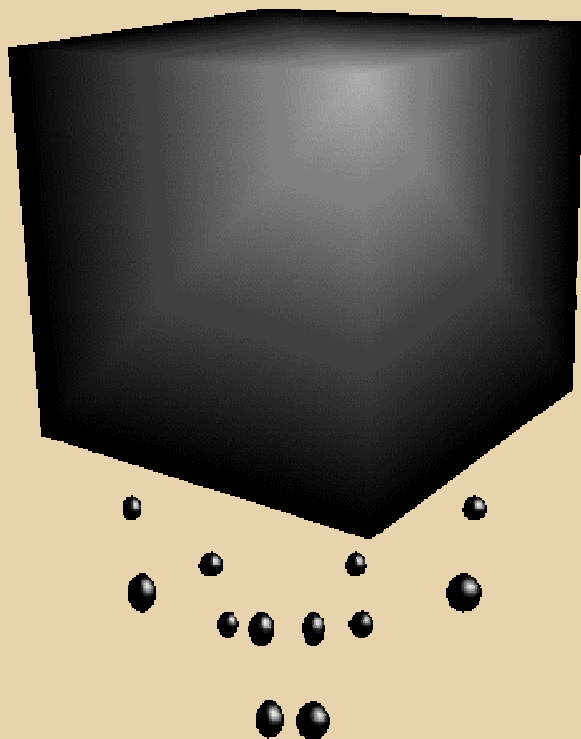


(Horizontal) SAGD:

- 85% sweep @ 10 years (typ.)
- $.85 * (.85-.15) = 60\%$ recovery

SAGD: "Reservoir" Steam/Oil Ratio

1 m³, 5 Darcy, 30% porosity:



Steam at 2250 kPa:

Temperature 10 → 225°C

Viscosity 10⁶ → 5 cp.

Oil Sat. 85% → 15%

Heat Required: 0.46 GJ

G/O fall velocity: 3.3 m/day

Oil Recovered: 1.3 bbl

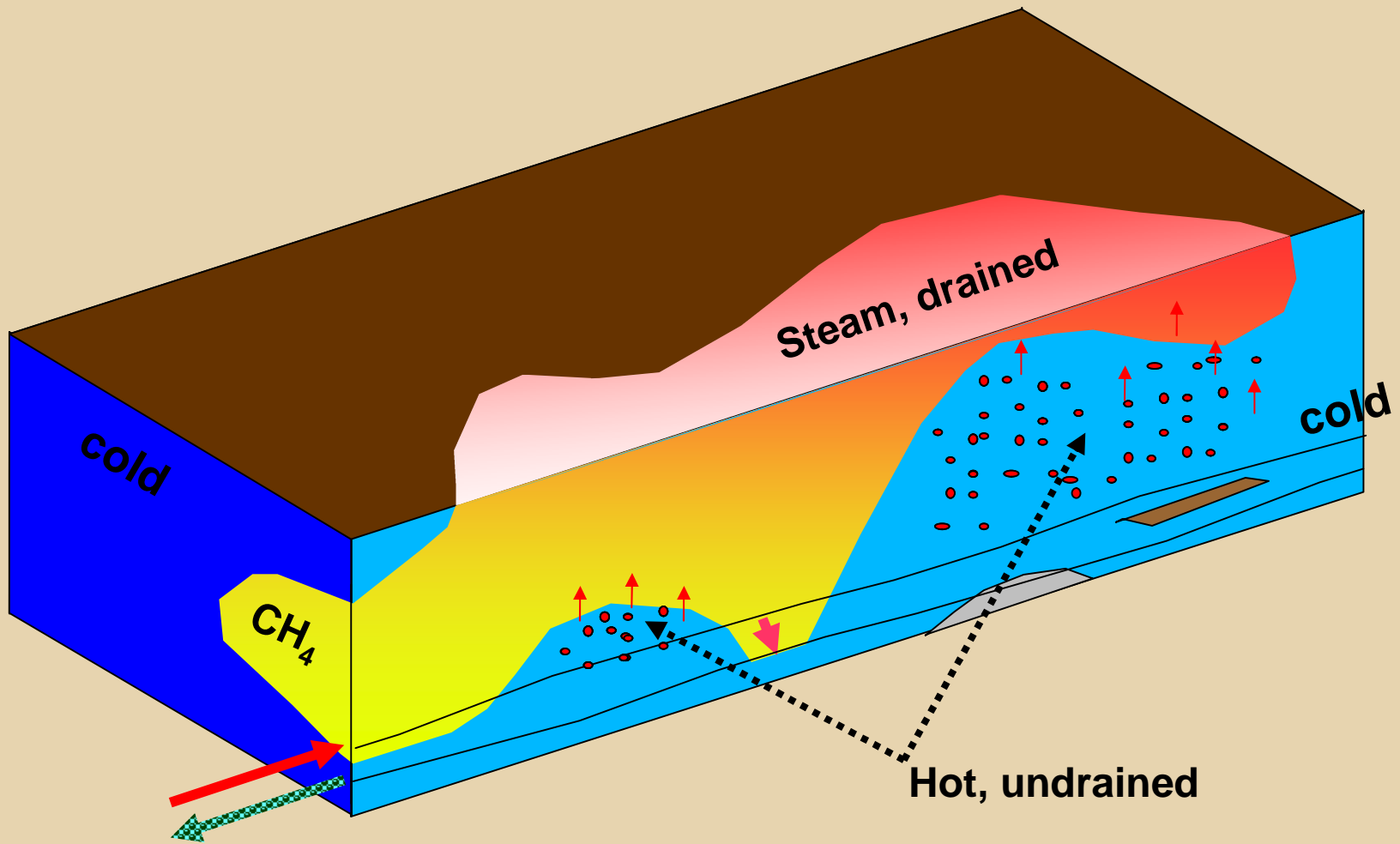
Equivalent SOR: 1.2

Real World SOR's & Heat Loss

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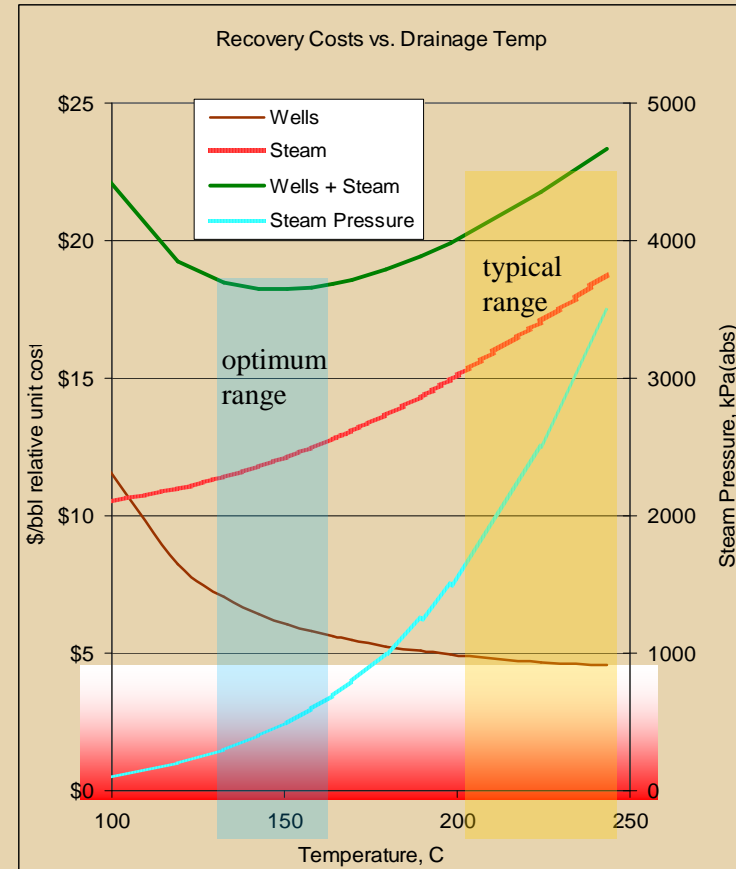
- **Current commercial SOR's are actually 2.5-3.5**
- **Excess steam consumption is due to heat loss to confining strata**
- **Heat losses are proportional to:**
 - *Steam temperature, i.e. pressure*
 - *Square root of the pattern operating lifetime*

Real World SAGD



Optimum SAGD

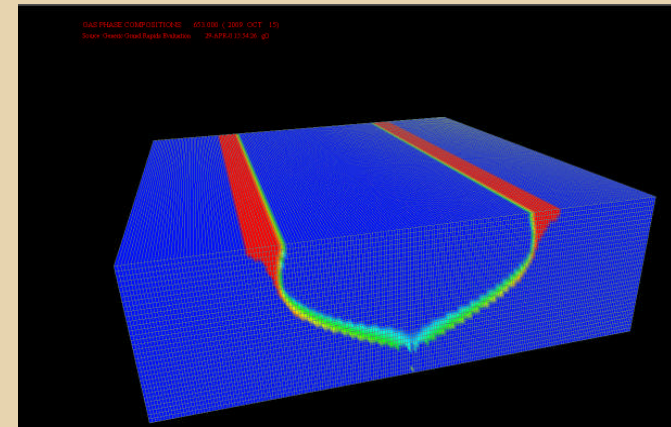
- under steady or cyclic operation, the rate of oil recovery is a function of the (time averaged) reservoir temperature
- in conventional SAGD, supply cost components of steam vs. wells is typically 3:1 or more
- lower temperature → lower SOR but less productive wells (same recovery, just slower)
- “save a lot on steam by spending a little more on wells”



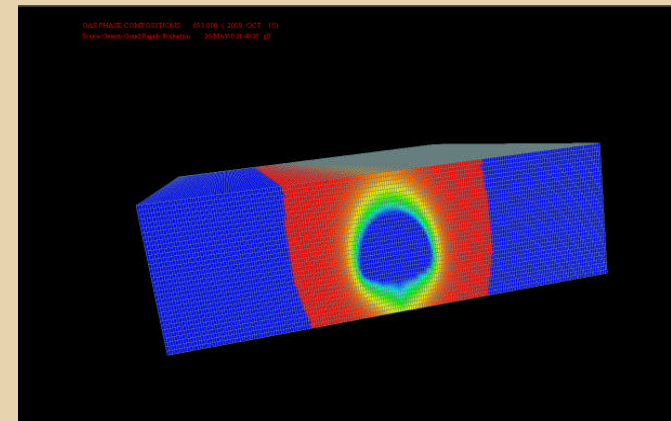
Cyclic SAGD

- ‘ideal’ optimum drainage temperature range is 100 - 150C (i.e. steam pressures 0 - 400 kPag)
- conventional SAGD needs \gg 500 kPag for well inflow & solution gas management
- cyclic steaming alternates:
 - short periods where steam fills the voidage and the sand is reheated; followed by
 - long production periods while oil drains due to stored heat; gas helps support the pressure.

Methane accumulation in SAGD



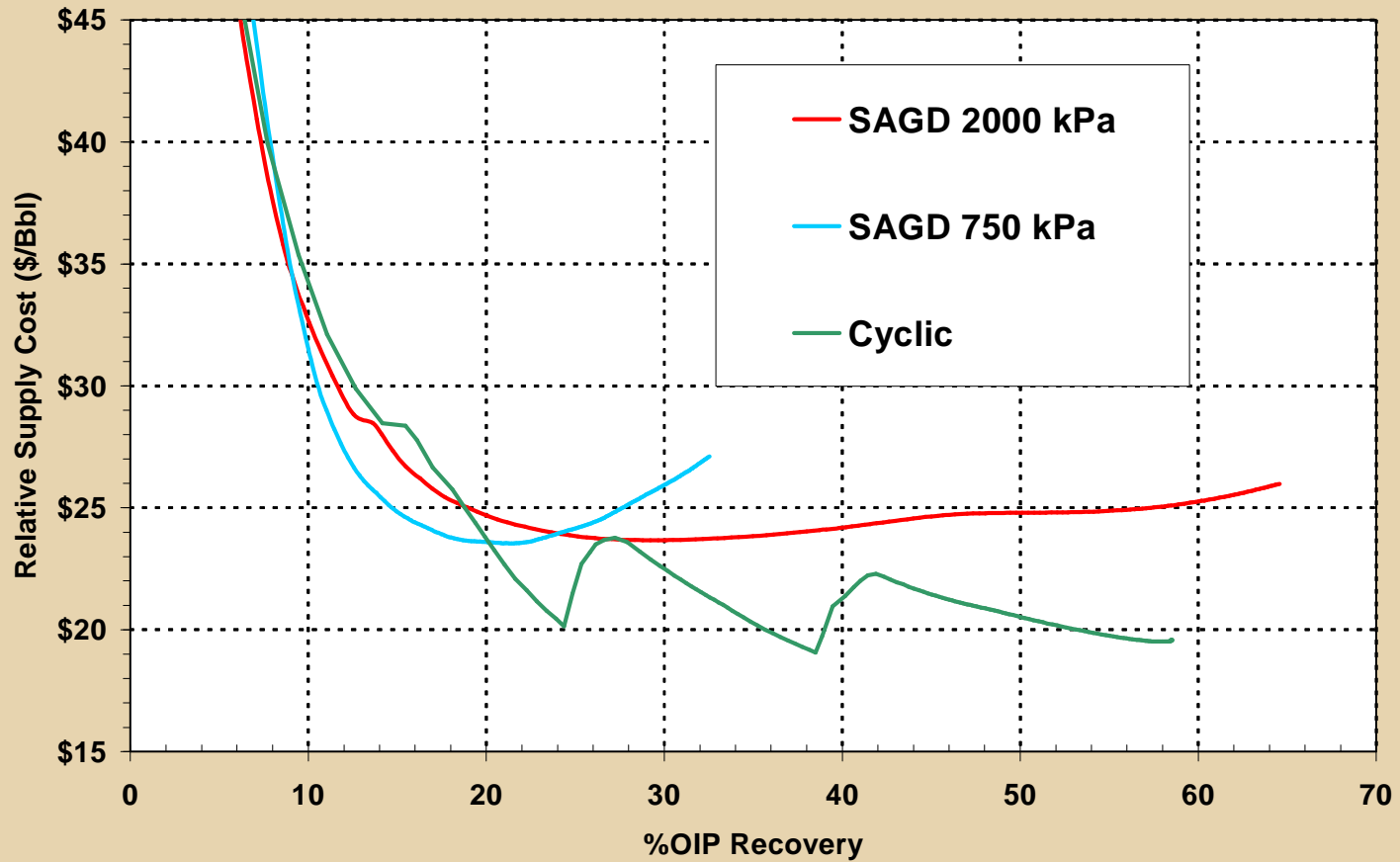
a) 2000 kPa



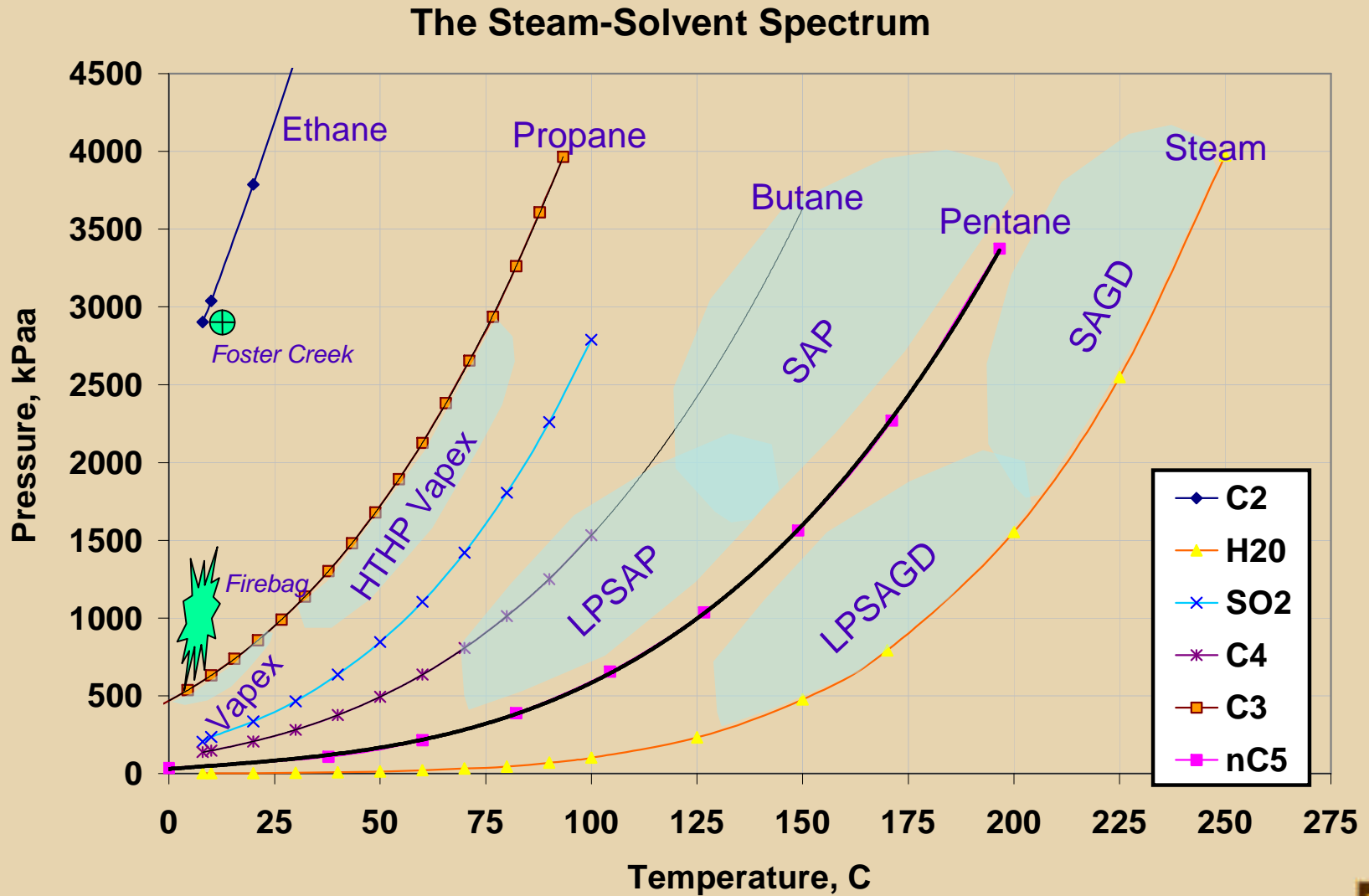
b) 750 kPa

Example Uplift - Cyclic Operation

- Thin Reservoir example:



The Steam-Solvent Spectrum



The Laricina Technology Suite

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- NC gas transport modelling
 - large impact on carbonates & LP, cyclic processes
- Cyclic steaming
 - lower (optimal) average res. temperature
 - temperature cycles, not necessarily pressure
 - twin or single
- Single wells
 - thin pay
 - startup by reservoir failure (geomechanics)
- Solvent additives
 - cyclic operation -> lower avg. inventory

Technologies for Reservoirs

Reservoir Type	Challenges	Approach(es)
thin (<20m)	<ul style="list-style-type: none"> • high SOR's • low OIP/pattern 	<ul style="list-style-type: none"> • single (horizontal) well cyclic • solvent additives • gas cycling
shallow (<100m)	<ul style="list-style-type: none"> • startup @/enforced low pressure • producer inflow 	<ul style="list-style-type: none"> • fracture, solvent, and/or electrical startup • colloid science,
complex (top gas, usually depressured, usually wet)	<ul style="list-style-type: none"> • enforced low pressure operation • losses to & encroachments from the cap 	<ul style="list-style-type: none"> • production inflow enhancements • repressurization w/air • dewatering

Conclusion

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- A first-principles approach to SAGD yields locally tailored and optimized recovery schemes
- There is a large opportunity in reducing the thermal intensity (average temperature) of conventional SAGD
- Cyclic steaming is key; solvent enhancements are a further opportunity to reduce temperature
- Laricina is advancing two pilot/prototypes and will solicit participants in June/July 2007